INVERSE PROBLEMS SHORT TUTORIAL: AN INTRODUCTION

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Concepts for inverse problems/parameter estimation problems illustrated by *examples*—Involves both *deterministic* and *probabilistic/stochastic/statistical* analysis Includes:

- Identifiability
- Ill-posedness
- Stability
- Regularization
- Approximation

SOME GENERAL REFERENCES:

JOURNALS:

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 - 2. H.T.Banks and K.Kunisch, Estimation Techniques for Distributed Parameter Systems, Birkhauser, Boston, 1989.
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- 6.H.W.Engl and C.W.Groetsch(eds.), *Inverse and Ill-posed Problems*, Academic, Orlando, 1987.
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FORWARD PROBLEM vs. INVERSE PROBLEM

Parameter dependent dynamical system:

$$\frac{dz}{dt} = g(t, z, \theta), \quad z(t_0) = z_0, \ g \text{ known, } \theta \in \Theta$$

 $z(t) \in R^K$, i.e., z(t) is a vector

Forward: Given θ , z_0 , find z(t) for $t \ge t_0$

Inverse: Given z(t) for $t \ge t_0$, find $\theta \in \Theta$

Mass-spring-dashpot system

$$m \frac{d^{2}x}{dt^{2}} + c \frac{dx}{dt} + kx = F$$

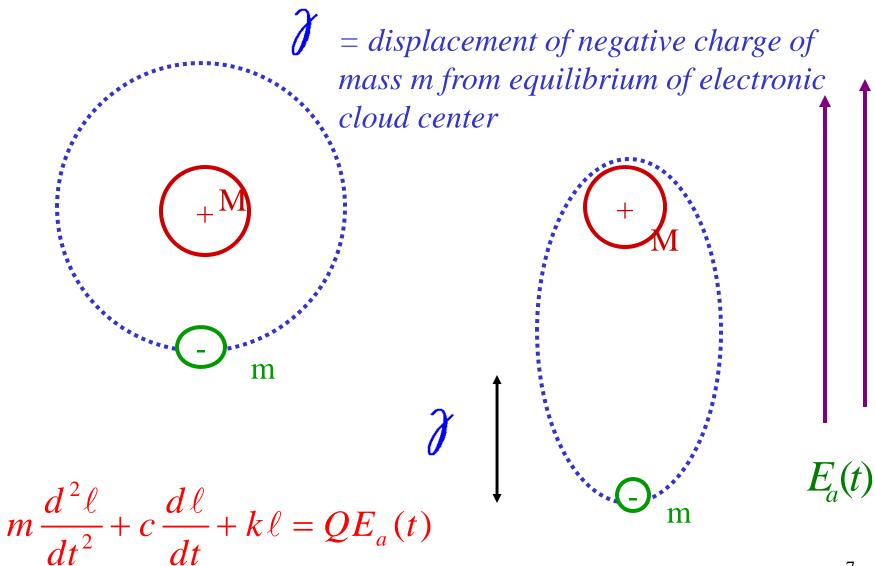
$$x(0) = x_{0} \frac{dx}{dt}(0) = v_{0}$$

$$x = equilibrium displacement of mass m$$

Forward: Given m, c, k, F, x_0, v_0 , find x(t) for $t > t_0$

Inverse: Given x(t) for $t \ge t_0$, v_0 , and F, find m, c, and k

Electronic Polarization—electronic cloud displacement



Usually are not given observations of all of system state z(t): Example(mass-spring-dashpot system):

First, rewrite as first order vector system:

$$z(t) = \begin{pmatrix} x(t) \\ dx(t) \\ dt \end{pmatrix}, \frac{dz(t)}{dt} = \mathcal{A}(\theta)z(t) + \mathcal{Z}(t), z_0 = \begin{pmatrix} x_0 \\ v_0 \end{pmatrix}$$

$$\mathcal{A}(\theta) = \begin{pmatrix} 0 & 1 \\ -\frac{k}{m} & -\frac{c}{m} \end{pmatrix} \quad \mathcal{Z}(t) = \begin{pmatrix} 0 \\ F(t) \\ m \end{pmatrix} \quad \theta = \left(\frac{k}{m}, \frac{c}{m}\right)$$

Observations:
$$f(t,\theta) = \mathcal{C} z(t,\theta)$$

Laser vibrometer:
$$f(t,\theta) = v(t) = \frac{dx(t)}{dt}$$

Observation operator: $\mathcal{C} = (0 \ 1)$

Proximity probe: $f(t,\theta) = x(t)$

Observation operator: $\mathcal{C} = (1 \quad 0)$

More likely, discrete (finite number) observations:

$$\left\{\tilde{y}_{j}\right\}_{j=1}^{n}$$
 where $\tilde{y}_{j} \approx f(t_{j}, \theta)$

Example: (from biology)
The *Logistic* population model (also called the *Verhulst-Pearl* growth model) is given by

$$\frac{dx(t)}{dt} = rx(t) \left(1 - \frac{x(t)}{K} \right), \ x(0) = x_0.$$

Here K is the *carrying capacity* as well as the asymptote value for solutions as t approaches infinity and r is the *intrinsic growth rate*.

Can formulate as least – squares fit of model to observations:

$$J(\theta) = \sum_{j=1}^{n} \left| \tilde{y}_j - f(t_j, \theta) \right|^2$$

where f is the model solution(response) or that part of the solution that we can "observe" or that we care about in design!

"Model driven" vs. "data driven" inverse problems

Model driven:
$$\tilde{y}_j = f(t_j, \theta)$$

Data driven: $\tilde{y}_j = f(t_j, \theta) + \varepsilon_j$, ε_j is error

(Depending on the error, may need to introduce variability into the modeling and analysis)

Model driven: $\tilde{y}_j = f(t_j, \theta)$

- i) System Design problems
 - a) design of spring / shock system (automotive, "smart" truck seats)
 - b) design of thermally conductive epoxies for use in computer motherboards
- ii) Nondestructive Evaluation (NDE) problems
 - a) thermal interrogation of conductive structures
 - b) eddy current based electromagnetic damage detection

Design of spring/shock system

Mass-spring-dashpot system

(automotive, "smart" truck seats) -

$$m\frac{d^2x}{dt^2} + c\frac{dx}{dt} + kx = F$$

$$x(0) = x_0 \quad \frac{dx}{dt}(0) = v_0$$

Choose $\theta = (k,c)$ to provide a given response x(t) for a "load" t and perturbation t

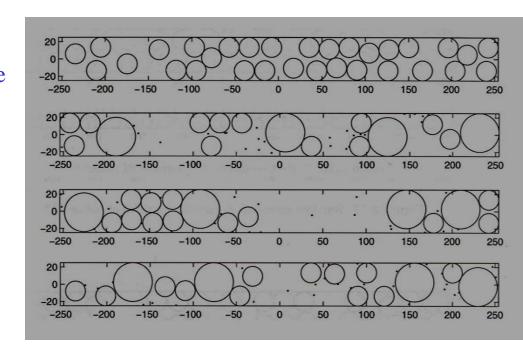
DESIGN OF THERMALLY CONDUCTIVE COMPOSITE ADHESIVES

GOALS

Design and analysis of thermally conductive composite adhesives (epoxies and gels filled with highly conductive particles such as aluminum, diamond dust, and carbon)

POTENTIAL AND SIGNIFICANCE

Development of enhanced thermally conductive adhesives for microelectronic devices, automotive and aeronautical components



Determine ρ, c_p , and k (all spatially varying) in

$$\rho(\vec{x})c_p(\vec{x})\frac{\partial u(t,\vec{x})}{\partial t} = \nabla(k(\vec{x})\nabla u(t,\vec{x}))$$

for a desired temperature u or flux $\frac{\partial u}{\partial n} = \nabla u \cdot \vec{n}$ on the boundary

References:

- 1) H.T.Banks and K.L.Bihari, Modeling and estimating uncertainty in parameter estimation, CRSC-TR99-40, NCSU, Dec.,1999; Inverse Problems 17(2001),1-17.
- 2) K.L.Bihari, Analysis of Thermal Conductivity in Composite Adhesives, Ph.D. Thesis, NCSU, August, 2001.
- 3) H.T.Banks and K.L.Bihari, Analysis of thermal conductivity in composite adhesives, CRSC-TR01-20, NCSU, August, 2001; Numerical Functional Analysis and Optimization, 23 (2002), 705-745.

Data driven: $\tilde{y}_j = f(t_j, \theta) + \varepsilon_j$, ε_j is error

Many (most!) of examples lead to the introduction of *variability* into both the modeling and the analysis!!

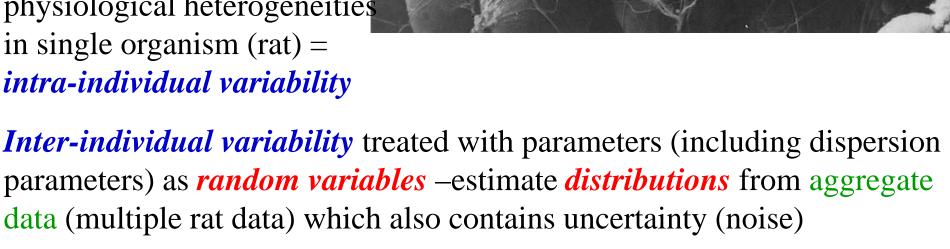
- i) Physiologically Based Pharmacokinetic(PBPK) modeling in toxicokinetics
- ii) Modeling of HIV pathogenesis

PBPK Models for TCE in Fat Cells

Millions of cells with varying size, residence time, vasculature, geometry:

"Axial-dispersion" type adipose tissue compartments to embody uncertain physiological heterogeneities in single organism (rat) =

intra-individual variability



Whole-body system of equations

$$V_{v} \frac{dC_{v}(t)}{dt} = Q_{f}C_{B}(t, \pi - \varepsilon_{2}) + \frac{Q_{br}}{P_{br}}C_{br}(t) + \frac{Q_{k}}{P_{k}}C_{k}(t) + \frac{Q_{f}}{P_{f}}C_{l}(t) + \frac{Q_{m}}{P_{m}}C_{m}(t) + \frac{Q_{c}}{P_{f}}C_{l}(t) - Q_{c}C_{v}(t)$$

$$C_{a}(t) = \left(Q_{c}C_{v}(t) + Q_{p}C_{c}(t)\right) / \left(Q_{c} + Q_{p}/P_{b}\right)$$

$$V_{br} \frac{dC_{br}(t)}{dt} = Q_{br}\left(C_{a}(t) - C_{br}(t)/P_{br}\right)$$

$$V_{B} \frac{\partial C_{B}}{\partial \phi} = \frac{V_{B}}{v_{2}} \frac{\partial}{\sin \phi} \frac{\partial}{\partial \phi} \left[\sin \left(\frac{D_{n}}{v_{2}}\right) \frac{\partial C_{B}}{\partial \phi} - vC_{B}\right] + \lambda_{l}\mu_{Bl}\left(f_{l}C_{l}(\theta_{0}) - f_{B}C_{B}\right) + \lambda_{l}\mu_{Bl}\left(f_{h}C_{h}(\theta_{0}) - f_{B}C_{h}\right)$$

$$V_{l} \frac{\partial C_{l}}{\partial t} = \frac{V_{l}D_{l}}{v_{l}^{2}} \left[\frac{1}{\sin^{2}\phi} \frac{\partial^{2}C_{l}}{\partial \theta^{2}} + \frac{1}{\sin\phi} \frac{\partial}{\partial \phi}\left(\sin\phi\frac{\partial C_{l}}{\partial \phi}\right)\right] + \delta_{\theta_{0}}(\theta)\chi_{B}(\phi)\lambda_{l}\mu_{Bl}\left(f_{B}C_{B} - f_{l}C_{l}\right) + \mu_{l}A\left(f_{h}C_{A} - f_{l}C_{l}\right)$$

$$V_{k} \frac{\partial C_{A}}{\partial t} = \frac{V_{k}D_{A}}{v_{0}^{2}} \left[\frac{1}{\sin^{2}\phi} \frac{\partial^{2}C_{A}}{\partial \theta^{2}} + \frac{1}{\sin\phi} \frac{\partial}{\partial \phi}\left(\sin\phi\frac{\partial C_{A}}{\partial \phi}\right)\right] + \delta_{\theta_{0}}(\theta)\chi_{B}(\phi)\lambda_{h}\mu_{Bl}\left(f_{B}C_{B} - f_{h}C_{A}\right) + \mu_{l}A\left(f_{l}C_{l} - f_{h}C_{A}\right)$$

$$V_{k} \frac{dC_{k}(t)}{dt} = Q_{k}\left(C_{a}(t) - C_{k}(t)/P_{k}\right)$$

$$V_{l} \frac{dC_{l}(t)}{dt} = Q_{l}\left(C_{a}(t) - C_{m}(t)/P_{m}\right)$$
Plus boundary conditions
$$V_{l} \frac{dC_{m}(t)}{dt} = Q_{l}\left(C_{a}(t) - C_{k}(t)/P_{l}\right)$$

and initial conditions

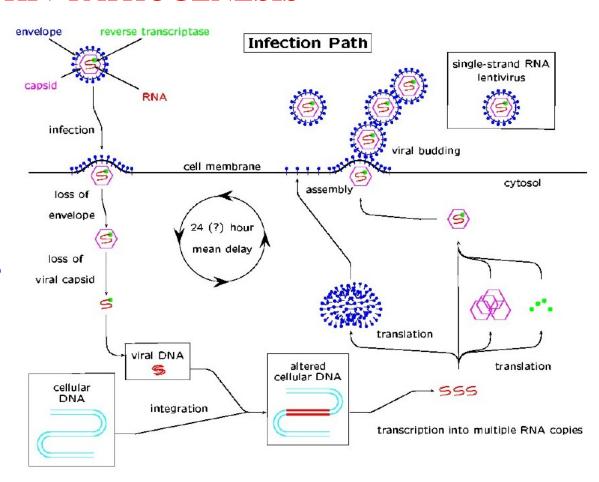
References:

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- 3)L.K.Potter, Physiologically based pharmacokinetic models for the systemic transport of Trichloroethylene, Ph.D. Thesis, NCSU, August, 2001
- 4)H.T.Banks and L.K. Potter, Model predictions and comparisions for three Toxicokinetic models for the systemic transport of TCE,CRSC-TR01-23,NCSU, August,2001; Mathematical and Computer Modeling 35(2002), 1007-1032
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MODELING OF HIV PATHOGENESIS

GOALS

DEVELOPMENT OF DYNAMIC MODELS INVOLVING INTRA-AND INTER-INDIVIDUAL VARIABILITY TO AID IN UNDERSTANDING OF FUNDAMENTAL MECHANISMS OF INFECTION AND SPREAD OF DISEASE-AGGREGATE DATA ACROSS POPULATIONS



POTENTIAL AND SIGNIFICANCE
POPULATION LEVEL ESTIMATION OF
SPREAD RATES AND EFFICACY IN
TREATMENT PROGRAMS FOR
EXPOSURE

Involves systems of equations of the form (generally nonlinear)

$$\frac{dV}{dt} = -cV(t) + n_a A(t-\tau) + n_c C(t) - n_{vt} V(t) T(t)$$

where τ is a production delay (distributed across the population of cells). That is, one should write

$$\frac{dV}{dt} = -cV(t) + n_a \int_0^\infty A(t-\tau)k(\tau)d\tau + n_c C(t) - n_{vt}V(t)T(t)$$

where k is a probability density to be estimated from aggregate data.

Even if **k** is given, these systems are nontrivial to simulate—require development of fundamental techniques.

HIV Model:

$$\dot{V}(t) = -cV(t) + n_A \int_{0}^{r} A(t-\tau) d\pi_1(\tau) + n_C C(t) - p(V,T)$$

$$\dot{A}(t) = (r_v - \delta_A - \delta X(t))A(t) - \gamma \int_0^r A(t - \tau)d\pi_2(\tau) + p(V, T)$$

$$\dot{C}(t) = (r_v - \delta_C - \delta X(t))C(t) + \gamma \int_0^r A(t - \tau)d\pi_2(\tau)$$

$$\dot{T}(t) = (r_u - \delta_u - \delta X(t))T(t) - p(V,T) + S$$

where $C(t) = E_2 \{C(t;\tau)\} = \int_0^r C(t;\tau) d\pi_2(\tau)$, A = acute cells

$$V(t) = V_A(t) + V_C(t), \ V_A(t) = E_1 \{V_A(t;\tau)\} = \int_0^t V_A(t;\tau) d\pi_1(\tau)$$

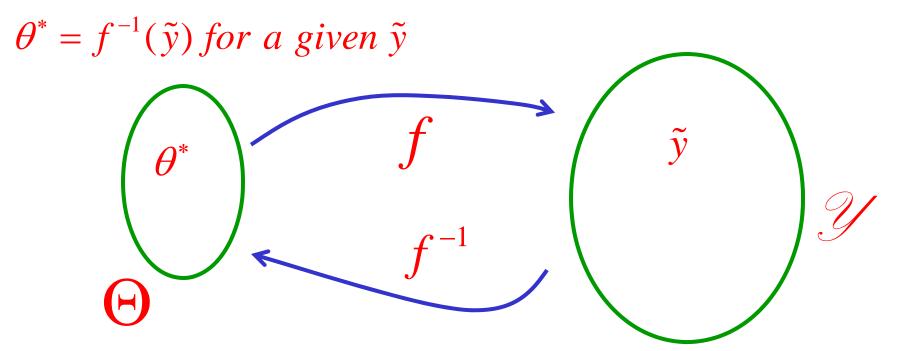
 $\pi_1 \leftrightarrow$ delay from acute infection to viral production $\pi_2 \leftrightarrow$ delay from acute infection to chronic infection T = target cells, X = total (infected+uninfected) cells

References:

- 1) D. Bortz, R. Guy, J. Hood, K. Kirkpatrick, V. Nguyen, and V. Shimanovich, Modeling HIV infection dynamics using delay equations, in 6th CRSC Industrial Math Modeling Workshop for Graduate Students, NCSU(July,2000), CRSC TR00-24, NCSU, Oct, 2000
- 2) H. T. Banks, D. M. Bortz, and S. E. Holte, Incorporation of variability into the modeling of viral delays in HIV infection dynamics, CRSC-TR01-25, Sept, 2001; Math Biosciences, 183 (2003), 63-91.
- 3) H.T.Banks and D.M.Bortz, A parameter sensitivity methodology in the context of HIV delay equation models, CRSC-TR02-24, August, 2002; J. Math. Biology, 50 (2005), 607--625.
- 4) D.M.Bortz, Modeling, Analysis, and Estimation of an In Vitro HIV Infection Using Functional Differential Equations, Ph. D. Thesis, NCSU, August, 2002.

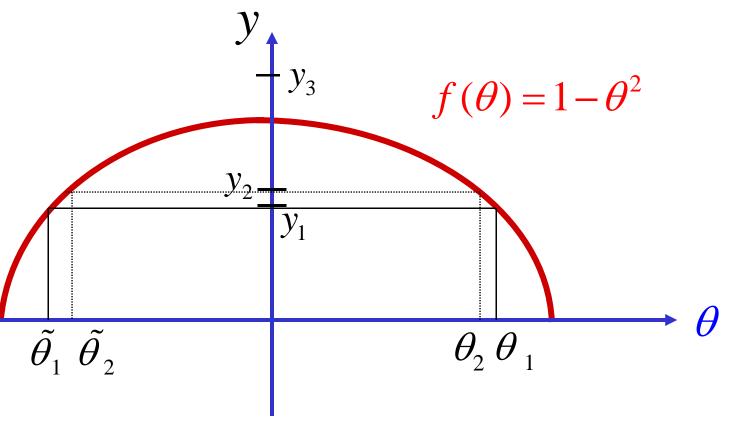
The problems above are (as are most others) notoriously *ill-posed*!! This concept is difficult to explain in the context of the problems outlined above—so we turn to some exceedingly simple examples to illustrate the ideas behind *well-posedness! Simplest case:*

one observation – \tilde{y} for $f(\theta)$ – and need to find preimage



Well-posedness:

- i. Existencei. Uniqueness
- ii. Continuous dependence of solutions on observations "stability" of inverse problem



Non-existence: No
$$\theta_3$$
 such that $f(\theta_3) = y_3$

Non-uniqueness:
$$y_j = f(\theta_j) = f(\tilde{\theta}_j)$$
 $j = 1, 2$

Lack of continuity of inverse map:

$$|y_1 - y_2|$$
 small \Rightarrow $|f^{-1}(y_1) - f^{-1}(y_2)|$
= $|\theta_1 - \tilde{\theta}_2|$ small

Why is this so important???

Why not just apply a good numerical algorithm for a least squares (for example) fit to try to find the "best" possible solution???? (Seldom expect zero residual!!)

Define
$$J(\theta) = |y_1 - f(\theta)|^2$$
 for a given y_1

and then apply a standard iterative method to obtain a solution!!

Iterative methods:

- 1) Direct search (simplex, Nelder-Mead,.....)
- 2) Gradient based (Newton, steepest descent, conjugate gradient,.....)

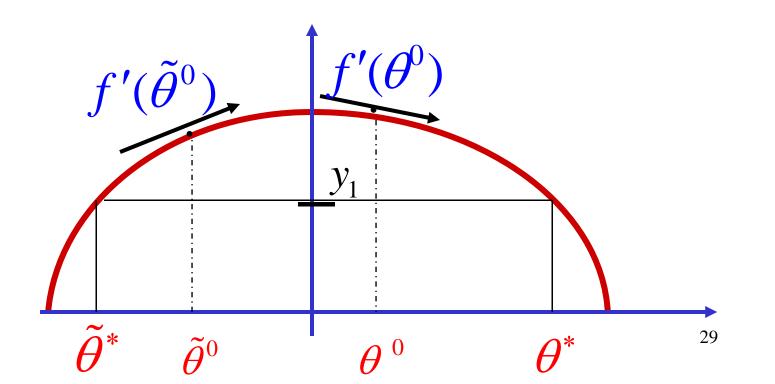
e.g., *Newton*:
$$\theta^{k+1} = \theta^k - [J'(\theta^k)]^{-1}J(\theta^k)$$

$$\theta^{k+1} = \theta^k - [J'(\theta^k)]^{-1}J(\theta^k)$$

For
$$J(\theta) = |y_1 - f(\theta)|^2$$
, $J'(\theta) = 2(y_1 - f(\theta))(-f'(\theta))$

$$J'(\theta^0) = 2(-)(--) < 0, \implies \theta^1 > \theta^0, \text{ etc.}$$

$$J'(\tilde{\theta}^0) = 2(-)(-+) > 0, \implies \tilde{\theta}^1 < \tilde{\theta}^0, \text{ etc.}$$



This behavior is not the fault of steepest descent algorithms, but is a manifestation of the inherent "ill-posedness" of the problem!!

How to fix this is the subject of much research over the past 40 years!! Among topics are:

i) constrained optimization { explicit(compact constraint sets) implicit(Lagrange multipliers)

ii) regularization
 (compactification, convexification)
 regularization
 regularization by discretization

Tikhonov regularization

Idea: Problem for $J(\theta) = |y_1 - f(\theta)|^2$ is ill – posed, so replace it by a "near – by" problem for

$$J_{\beta}(\theta) = |y_1 - f(\theta)|^2 + \beta |\theta - \theta_0|^2$$

where β is a regularization parameter to be

"appropriately chosen" !!

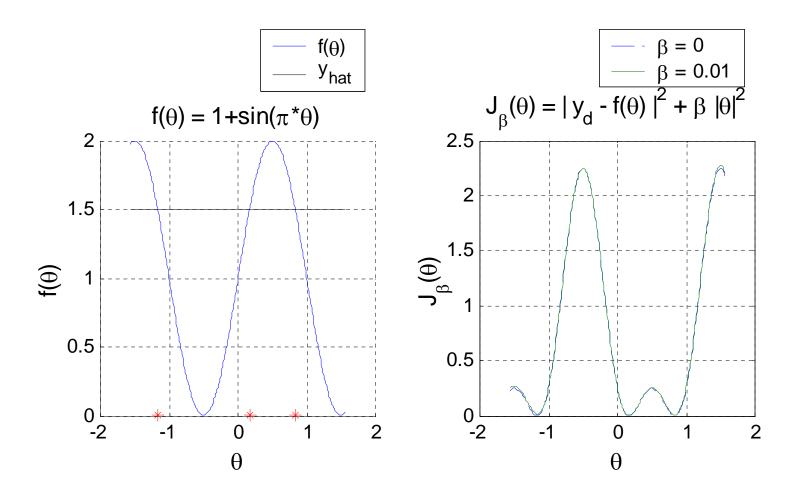
PRO: When done correctly, provides convexity and compactness in the problem!

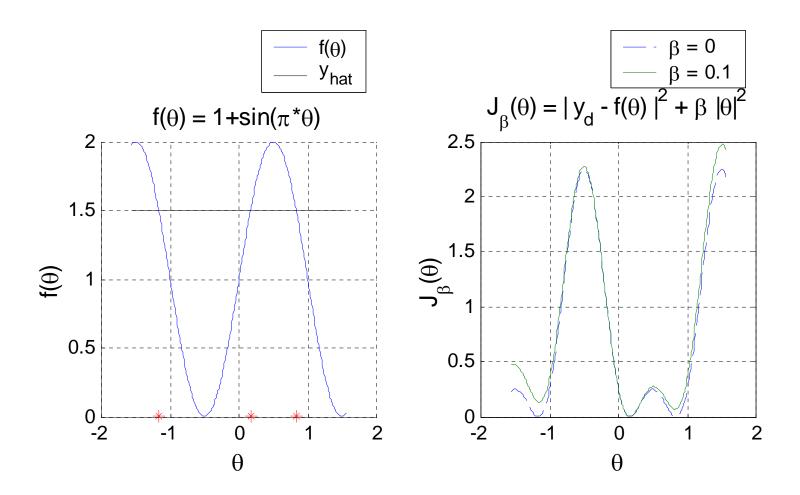
CON: Even when done correctly, it changes the problem and solutions to the new problems may not be close to those of original! Moreover, it is not easy to do correctly or even to know if you have done so!!

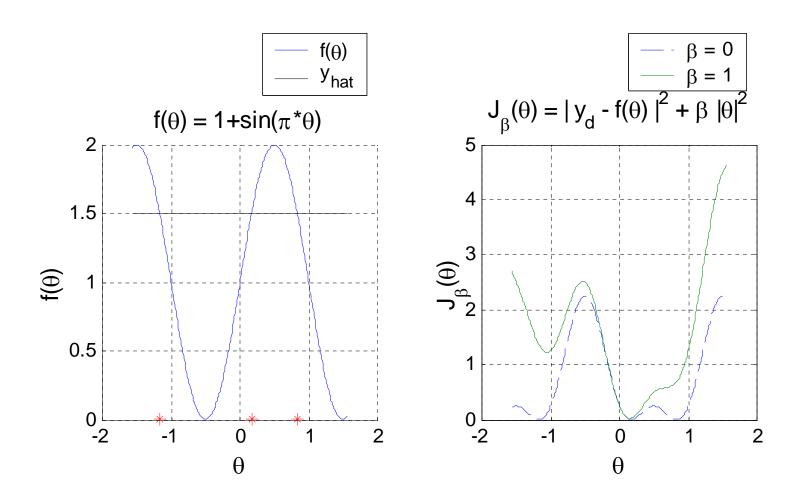
EXAMPLE:

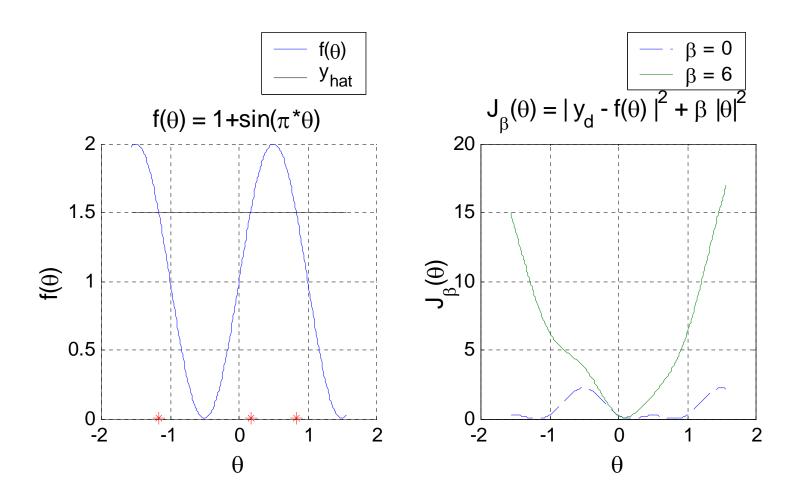
 $f(\theta) = 1 + \alpha \sin(\pi \theta)$, β ranging from $\beta = 0$ to 100 thru values 0, .01,...,1.0,...,10,...,40,...,80, 100, several values of α , θ_0 , and y_1

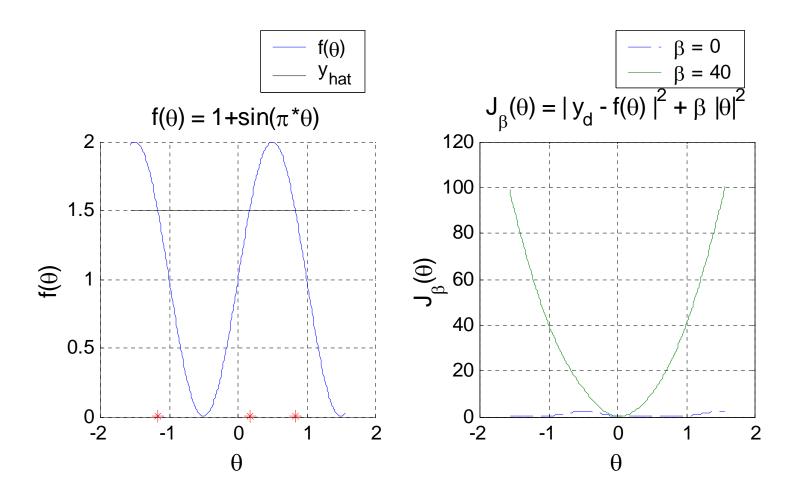
- 1) $\alpha = 1$, $y_1 = 1.5$, $\theta_0 = 0$ (tik)*
- 2) $\alpha = .5$, $y_1 = .8$, $\theta_0 = 0$ (tik1)
- 3) $\alpha = .5$, $y_1 = 1.6$ (not in range of f), $\theta_0 = 0$ (tik2)*
- 4) $\alpha = 1, y_1 = 1.5, \theta_0 = 1.0$ (tik4)
- 5) $\alpha = 1, y_1 = 1.5, \theta_0 = 1.8$ (tik6)*
- 6) $\alpha = 1, y_1 = 1.5, \theta_0 = .5$ (tik7)*
- 7) $\alpha = 1, y_1 = 1.5, \theta_0 = -.5$ (tik8)*









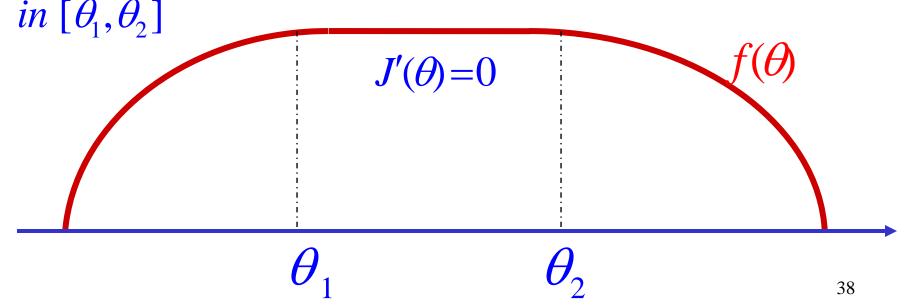


SENSITIVITY

How does $f(t,\theta) = \mathcal{C} z(t,\theta)$ change with respect to θ and how does this affect the effort to minimize

$$J(\theta) = |y_1 - f(\theta)|^2 ??$$

Recall that $J'(\theta) = 2(y_1 - f(\theta))(-f'(\theta))$ and Newton $\theta^{k+1} = \theta^k - [J'(\theta^k)]^{-1}J(\theta^k)$ stalls for initial values



So we are interested in $\frac{\partial f}{\partial \theta} = \mathcal{C} \frac{\partial z}{\partial \theta}$ which is obtained from general sensitivity theory:

Example: For
$$\frac{dz}{dt} = g(t, z, \theta)$$
, we find $s(t) \equiv$

$$\frac{\partial z(t,\theta^*)}{\partial \theta} \quad satisfies \quad \frac{ds(t)}{dt} = \left(\frac{\partial g}{\partial z}\right)^* s(t) + \left(\frac{\partial g}{\partial \theta}\right)^*$$

where
$$\left(\frac{\partial g}{\partial z}\right)^* = \frac{\partial g}{\partial z}(t, z(t, \theta^*), \theta^*),$$

$$\left(\frac{\partial g}{\partial \theta}\right)^* = \frac{\partial g}{\partial \theta}(t, z(t, \theta^*), \theta^*)$$

APPROXIMATION/COMPUTATIONAL ISSUES

As we have noted, most observations have the form $f(t,\theta) = \mathcal{C} z(t,\theta),$

where z is the solution of an ordinary or partial differential equation. In general, one cannot obtain these solutions in closed form even if θ is given. Thus one must turn to approximations and computational solutions.

For example, in the case of z satisfying an ODE

$$\frac{dz}{dt} = g(t, z, \theta),$$

one can apply finite difference techniques to discretize the system, obtaining an algebraic system for $z_k^N \approx z(t_k)$ given by

$$z_{k+1}^{N} = g^{N}(z_{0}^{N}, z_{1}^{N}, ..., z_{k}^{N}, \theta).$$

e.g., Runge – Kutta, predictor – corrector, stiff methods of Gear

Thus, one must use

$$f_{k}^{N}(\theta) = \mathcal{C} z_{k}^{N}(\theta)$$

in

$$J^{N}(\theta) = \sum_{j=1}^{n} \left| \tilde{y}_{j} - f_{j}^{N}(\theta) \right|^{2}$$

which yields solutions $\hat{\theta}^{N}$.

Question: What is relationship of $\hat{\theta}^N$ to $\hat{\theta}$??? Convergence, preservation of stability, sensitivity, well posedness, etc., of problems, solutions???

In the case of partial differential equation systems, one can introduce finite difference or finite element approximations.

Example: Finite elements ("linear elements") in dispersion equations—heat, population dispersal, molecular diffusion, etc.

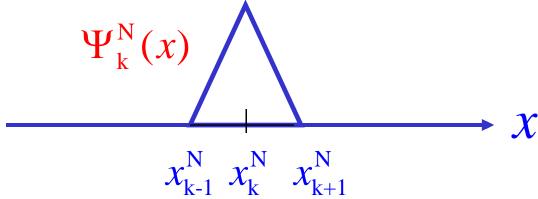
$$\frac{\partial u(t,x)}{\partial t} = \frac{\partial}{\partial x} \left(\theta(x) \frac{\partial u(t,x)}{\partial x} \right) + F(t,x)$$

Idea: Look for approximate solutions of the form

$$u^{N}(t,x) = \sum_{k=1}^{N} z_{k}^{N}(t) \Psi_{k}^{N}(x)$$

for a given set of basis elements $\left\{\Psi_{k}^{N}\right\}_{k=1}^{N}$, leading to a system for $z^{N}(t) = (z_{1}^{N}(t), z_{2}^{N}(t), ..., z_{N}^{N}(t))$ to be used in $f^{N}(t,\theta) = \mathcal{C}^{N}z^{N}(t,\theta)$.

Linear Elements



leads to finite dimensional system

$$\frac{dz^{N}(t)}{dt} = \mathcal{A}^{N}(\theta)z^{N}(t) + \mathcal{Z}^{N}(t)$$

where

$$\mathcal{A}^{N}(\theta) = \left(\int \theta(x) \Psi_{i}^{N}(x)' \Psi_{j}^{N}(x)' dx\right)$$

Finite elements generally result in large (dimension $\sim 10,000-20,000$) approximating systems!! These can be extremely time consuming in inverse problem calculations. So there is great interest in *model reduction* techniques that will result in substantial reduction in time! To illustrate one such technique (Proper Orthogonal Decomposition), we return to the eddy current based NDE example.

SUMMARY REMARKS

- 1. Two classes of problems (model/design driven-no data, and data driven)
- 2. In both classes, may need to introduce *variability/un-certainty* (recall PBPK, HIV examples) even when considering simple case of a single individual
- 3. If design/model driven efforts are successful (recall eddy current NDE example), most likely will lead to validation experiments, data, and necessitate development of statistical models
- 4. There are significant issues, challenges, and methodology (well-posedness, regularization, approximation/computation, model reduction, etc.) that are important to consider in both classes of problems!